

# Tribological Characterization of Inconel 718 under Varying Load Conditions

ZUHA SHAFI WANI<sup>1</sup> MANISH KUMAR GUPTA<sup>2</sup>

<sup>1</sup> M. tech scholar, Department of Mechanical Engineering, RIMT University, Mandi Gobindgarh Punjab,

<sup>2</sup> Assistant professor, Department of Mechanical Engineering, RIMT University, Mandi Gobindgarh Punjab.

---

## ABSTRACT

Inconel 718 are commonly used in gas turbine engines in those areas of the engine that are subjected to high temperatures and which requires high strength, excellent creep resistance, as well as corrosion and oxidation resistance. In this work the samples were prepared by powder metallurgy process and then the effect of load on the friction and wears behaviour of prepared Inconel 718 against silicon carbide balls sliding wear tests in air medium were studied. Rotary tests using a ball-on-disc type setup were conducted under various applied normal loads in order to measure friction coefficient and wear rates. Moreover, the analysis of surface morphology was done by using Optical Microscopy, SEM, and 3D-Surface Profilometer.

**Keywords:** Tribology, super alloys, Inconel 718, Silicon Carbide, load tests.

---

Date of Submission: 11-01-2023

Date of acceptance: 27-01-2023

---

## I. INTRODUCTION

Tribology is derived from the Greek phrase “tribos” meaning “rubbing or sliding”. Tribology can be described because the technology and technology of interacting surfaces in relative movement. Tribology includes the separate components of friction, put on and lubrication, which become as soon as treated one after the opposite. As those three components are interrelated, it's far larger to deal with them collectively as far as viable. Tribology is a location of generation which applies an operational evaluation to troubles of superb financial importance which includes reliability, protection and put on of technical equipment's starting from spacecraft to circle of relative's domestic system [1].

Put on is a removal of material from the operating surfaces below the mechanical movement of the 2 surfaces rubbing collectively. Relative movement amongst device components nearly inevitably leads to adjustments inside the floor of engineering additives which degrades the performance and lifetime of mechanical additives and consequences in monetary loss. Put on can also occur in some of modes that is composed of erosion, adhesion and erosion encompassing the world of tribology [2]. Excessive temperature placed on is one of the existences limiting elements whilst metallic surfaces are in repeated contact [3]. High forming temperatures impact the wear and tear and tear behaviour of equipment thru loss of mechanical energy and superior oxidation [4]. It's miles well known that oxidation ends in material degradation and consequently reduces the fabric resistance to position on. However, a floor oxide can also lessen the oxidation fee and help to lower the damage and tear loss if it's miles dense and robust [5]. Excessive-temperature alloys have been used extensively within the fuel turbine engines, plane, turbine disk, blades and combustor within the aerospace industry and steam power plants due to the aggregate in their mechanical houses and resistances to excessive temperature and corrosion. A few excessive-temperature alloys had been used in place of metal to resist the thermal fatigue in some key projects in present day years, which conjures up the investigations on their sliding behavior and put on mechanism [6].

## II. SUPER ALLOYS

Fantastic alloys are commonly utilized in fuel turbine engines in the ones regions of the engine which might be subjected to high temperatures and which requires excessive power, brilliant creep resistance, as well as corrosion and oxidation resistance. In turbine engines that is in the high strain turbine wherein blades can face temperatures drawing near if no longer beyond their melting temperature. New jet engines aren't green due to higher working temperatures, requiring higher – acting components. The use of superb alloys can permit the working temperature to be multiplied from 1200F to 1300F. Besides increasing performance and power output, higher temperature consequences in decreased emissions because the combustion cycle is extra entire. Super alloys are the high-temperature substances which display splendid resistance to mechanical and chemical degradation at temperatures near its melting points. Super alloys are mainly divided into three categories nickel-base super alloys, cobalt-base super alloys, and iron- base super alloys. The bodily, mechanical, and machining

behaviour of each organization varies considerably due to the chemical compositions of the alloy and the metallurgical processing it gets for the duration of manufacturing. Incredible alloys are also classified into wrought, cast, and powder metallurgy (PM) excellent alloys. The wrought can be strong answer reinforced or precipitation hardened alloys. These are usually diagnosed through exchange names or with the aid of unique numbering structures. Suitable compositions of extremely good alloys may be solid, rolled into sheets/bars, or otherwise produced in a variety of shapes. Bar and plate inventory materials are the very best shape of uncooked substances to cope with [7]. Brilliant alloys usually include Ni, Cr, Co, Mo, and Fe as main alloying elements. Others are Al, W, Ti, and so on. The position of those alloying factors is to beautify the traits of first-rate alloys inside the following manner Ni stabilizes alloy structure and homes at excessive temperatures. Co, Mo, and W growth energy at increased temperature. Cr, Al, Si enhance resistance to oxidation and provide high temperature corrosion. C increases creep energy [8].

### III. COMPOSITION

The composition of nickel-primarily based super alloys is altered relying on the preferred homes. Besides nickel, the alloys incorporate in general 10-20 % chromium, up to 8 % aluminium collectively with titanium, and 5-10 % cobalt. Small quantities of boron, zirconium and carbon are covered as properly. Common place addition in some alloys is as an example molybdenum, tungsten, niobium, tantalum and hafnium. There are also some tramp elements, i.e. factors which by accident had been included within the alloy, and those factors ought to be carefully controlled. Examples of factors belonging to this organization are silicon, phosphorus, sulphur, oxygen and nitrogen. Chromium and aluminium are preferred due to the fact they enhance the oxidation resistance of the alloy. A small quantity of yttrium binds the oxide layer to the substrate. Boron and zirconium are delivered to the polycrystalline super alloys wherein they segregate to the grain boundaries. This effects in a better creep power and ductility. The carbides generally tend to precipitate on the grain boundaries and prevent the sliding phenomenon of the limits. Some examples of carbide formers are carbon, chromium, molybdenum and tungsten. Some elements function as strong-solution strengthens, e.g. cobalt, iron, niobium, rhenium and molybdenum. The addition of titanium will growth the new corrosion resistance and the position of nickel is to present section balance. Super alloys are analysed in various applications. But my thesis paintings are on cloth Inconel 718, Nimonic 80A and silicon carbide and the information of cloth are beneath under.

### IV. INCONEL 718

The improvement of super alloys has significantly contributed to the development of fuel turbine jet engines utilized in aeronautic industry. Super alloys made with 80% nickel and 20% chromium were evolved inside the first half of the 20th century and could help combustion temperatures as high as 780oC when alloyed with small quantities of aluminium and titanium. Those alloys were further optimized inside the 1950's with the creation of vacuum melting and vacuum arc melting technologies imparting a higher manage inside the alloy chemistries and as a consequence enhancing the mechanical homes. The Inconel 718 alloys have been evolved within the 1960's as a brand-new class of super alloys containing a large fraction of niobium and tantalum for the precipitation of a second segment with excessive hardenability. The Inconel 718 alloys are generally produced by means of casting, homogenization and warm-forging. Inconel alloys 718 is an excessive-electricity, corrosion- resistant nickel chromium fabric used at -423 to 1300 off. The age-hard enable alloy can be with ease fabricated, even into complex elements. Its welding traits, specially its resistance to post weld cracking, are terrific. The clean and financial system with which Inconel alloy 718 can be fabricated, blended with right tensile, fatigue, creep, and rupture strength, have led to its use in an extensive range of software.

### V. Chemical composition and physical constants of Inconel 718

*Table 1 Chemical Composition (in weight %) of the Inconel 718*

Ni	Fe	Cr	Mo	Nb+Ta	Ti	Al	Co
55	12.2	21	3.3	5.5	1.2	0.8	1

**Table 2** Physical constants of Inconel 718

Constants	Density gm.cm <sup>-3</sup>	Melting Temp.(°C)	Thermal Conductivity (W/m*K)	Electrical Resistivity, (μΩ*m)	Specific heat (J/kg*K)
Value	8.470	1277	11.4	1.25	435

**Table 3** Mechanical properties of Inconel 718

Properties	Hardness	Young's modulus (GPa)	Tensile Strength (MPa)
Value	42 HRC	206	1375

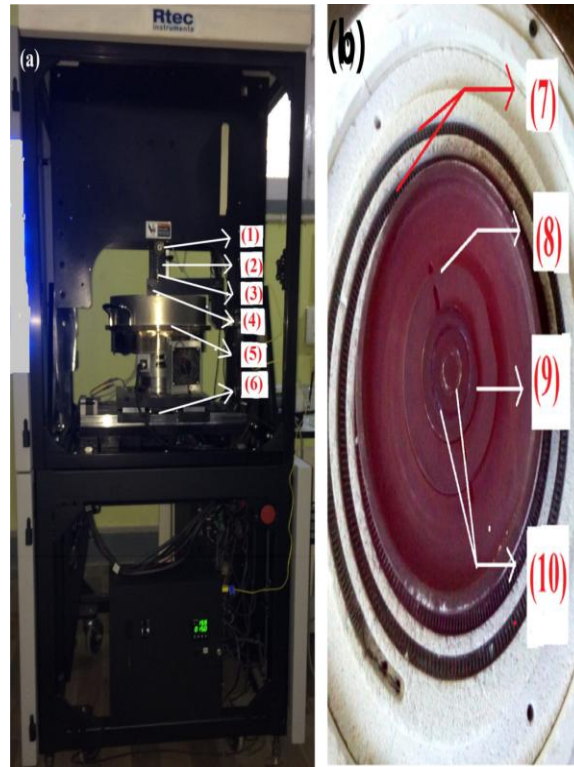
## VI. METHODOLOGY

### SAMPLE PREPARATION

Inconel 718 and Silicon carbide had been used for each test carried out. Inconel 718 and Silicon carbide materials were procured from Bharat Aerospace metals, India, Inconel 718 Ni changed into procured inside the shape of rods of 30mm diameter. Then rods were cut into discs of dimension 30 mm diameters x nine mm thickness.

### TRIBOLOGICAL TESTS

Tribological attempting out uses tribometer or devices to diploma wear and friction. Tribometer is a device as demonstrated in figure1, for studies of tribological homes. Tribometer is based at the motion of sliding between the surfaces and references (table bound ball on rotating disc) and the testing is performed underneath the managed conditions of sliding, load, temperature, humidity and in order those factors strongly have an effect at the tribological houses. The simple functions of all of the tribometers include the device affords motion, enforcing load and some form of adapter that may hit upon and convert the physical values of sorting out into anticipated values. Considering that our critical situation changed into to examine the un-lubricated friction and put on of the Inconel 718 samples in competition to silicon carbide. Such check system like rotary check rig became enough to serve the motive.



**Figure 1:** (a) Schematic representation of high-precision tribological test rig: (1) Load actuator, (2) spring, (3) ball holder, (4) load sensor, (5) closed heating chamber, (6) X–Y platform, (b) inside view of closed heating chamber at 450 °C (7) Heating coils, (8) sample's holder, (9) sample, (10) wear scar.

**EXPERIMENTAL PROCEDURE**

Great studies on the friction and put on checks have been finished beneath dry situations (in an effort to take away the contribution of lubricant) on a pc managed prevalent tribometer sliding test rig on a ball-on-discs configuration underneath a rotary motion with a point touch put on mode. The balls live over the discs with two degree of freedom: a vertical one, which lets in normal load application by direct contact with the surface of the disc, and a horizontal one, for friction measurement. The ball stationary over the rotating Inconel 718 disc, the rotation of disc underneath the test situations gives the friction coefficient curve that become recorded robotically by using a computer this is attached to widespread tribometer. For comparative reasons, all of the load tests were done with identical experimental parameters. Load tests were achieved on the regular load of 10 N, 20 N, 30N and 40 N. The sliding distance and temperature were stored consistent. Coefficient of friction and wear price were measured after each load take a look at.

**CALCULATION OF WEAR VOLUME AND WEAR RATE**

Put on charge of disc changed into measured with the assist of damage scar diameter from optical microscope and intensity, width from the 3D-profilometer. In tribological research in which many specimens need to be analysed, a technique is required for price willpower that's as easy and as rapid as possible. The use empirical equation where  $V_w = \pi d \times y \times z$ ,  $V_w$  is the wear and tear extent,  $d$  is the damage scar diameter of disc and  $y$  and  $z$  is width and depth of wear and tear scar. An easy optical microscope may be used to achieve the dimensions of the wear scar. The wear scar can be used to calculate the damage quantity.

Wear rate of the disc is obtained by Archard wear model equation (3.1)

$$K_w = \frac{V_w}{P \times D_s} \dots \dots \dots (3.1)$$

Where,  $K_w$  = Wear rate ( $\text{mm}^3/\text{N}\cdot\text{m}$ )

$V_w$ = Wear volume ( $\text{mm}^3$ );  $D_s$  = Sliding distance (m);  $P$ = Normal load (N)

The wear volume of ceramic SiC ball of diameter 10 mm was calculated from wear scar diameter using the following equations:

$$\text{Wear Volume} = \pi h^2 (r - h/3) \dots\dots\dots (1)$$

$$\text{Scar depth, } h = \frac{(d/2)^2}{r + \sqrt{r^2 - (d/2)^2}} \dots\dots\dots (2)$$

$$K_w = V_w / D_s \times P \text{ (mm}^3 \text{ N}^{-1} \text{ m}^{-1}) \dots\dots\dots (3)$$

Where;  $K_w$ = Specific Wear Coefficient ( $\text{mm}^3 \text{N}^{-1} \text{m}^{-1}$ ),  $V_w$  =Wear Volume ( $\text{mm}^3$ ),  $D_s$ =Sliding Distance (m),  $P$ = Normal load (N),  $r$  is radius of the ball;  $d$  is diameter of wear scar.

## VII. RESULTS

The details of the experimental parameters, data and calculated data can be found in the following table:

**Table 4: Load tests: Inconel 718**

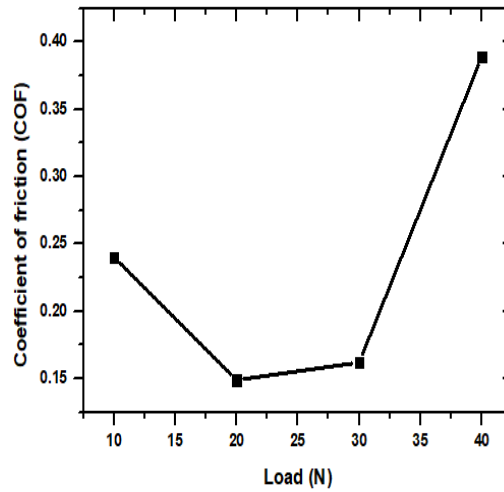
		Test 1	Test 2	Test 3	Test 4
Disc		Inconel 718	Inconel 718	Inconel 718	Inconel 718
Ball		SiC	SiC	SiC	SiC
Load (N)		10	20	30	40
Temperature( $^{\circ}\text{C}$ )		450	450	450	450
Sliding Distance(m)		200	200	200	200
RPM		133	133	133	133
Velocity(m/s)		0.111	0.111	0.111	0.111
Track Dia (mm)		12	12	12	12
Time (min)		30	30	30	30
File Name		y5-450t-80a-10n	y1-718-20n	y2-80a-30n2	y3-718-40n
COF		0.2402	0.1490	0.1621	0.3890
DISC	Wear volume( $\text{mm}^3$ )	3.00622	1.61223	4.14173	3.91316
	Wear rate( $\text{mm}^3/\text{Nm}$ )	$1.50031 \times 10^{-3}$	$0.70305 \times 10^{-3}$	$0.6902 \times 10^{-3}$	$0.48914 \times 10^{-3}$
BALL	Wear volume( $\text{mm}^3$ )	$5.6432 \times 10^{-3}$	$3.3849 \times 10^{-3}$	$5.8089 \times 10^{-3}$	$0.015624 \times 10^{-3}$
	Wear rate( $\text{mm}^3/\text{Nm}$ )	$2.8216 \times 10^{-6}$	$0.8462 \times 10^{-6}$	$0.9681 \times 10^{-6}$	$1.9530 \times 10^{-6}$

### TRIBOLOGICAL TESTS

The tribological behaviour of Inconel 718 was studied under dry unlubricated conditions the usage of the ball on disc configuration defined in previous bankruptcy. Each the friction and wear of the substances had been studied. The test situations were various to analyse the impact of load, on tribological behaviour. To permit the comparisons, samples were examined beneath same situations.

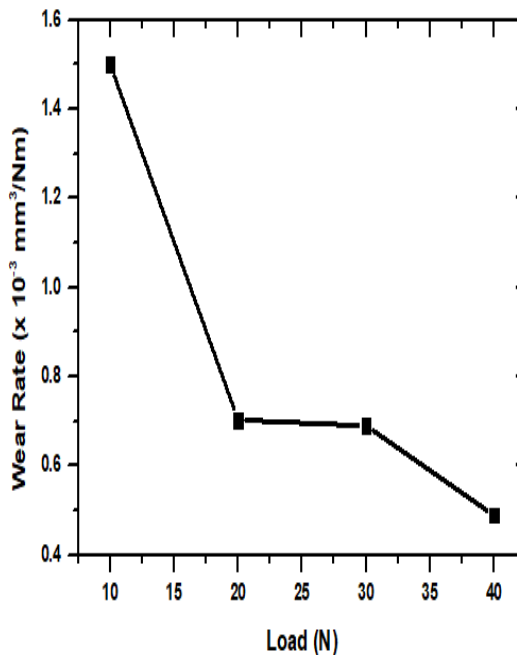
**LOAD TESTS**

The table 4 represents the facts that gives the variant of coefficient of friction of Inconel 718 against silicon carbide beneath same check situations. The table 4 represents the version of COF with increasing load. The variety of COF for Inconel 718 in opposition to silicon carbide is in among 0.2402-0.3890. The value of COF for Inconel 718 against silicon carbide at 10 N is 0.2402. Because the load will increase from 10 N to 20 N price of COF decreases, Inconel 718 towards silicon carbide from 0.2402 to 0.1490. Because the load in addition increases from 20 N to 40 N price of COF will increase from 0.1490 to 0.3890.



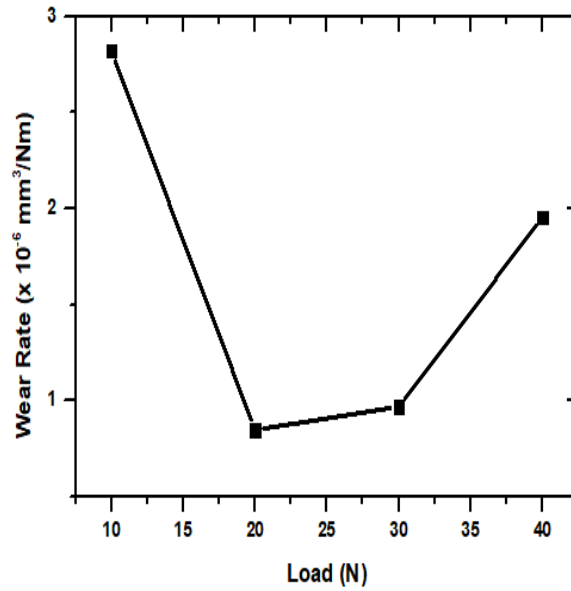
**Figure 2:** Coefficient of friction as a function of load

The table 4 additionally represents the information that offers the version of wear and tear price of Inconel 718 towards silicon carbide under same take a look at situations. The range of damage price for Inconel 718 towards silicon carbide is in among  $(1.50-0.48) \times 10^{-3} \text{mm}^3\text{N}^{-1}\text{m}^{-1}$ . Most wear charge occur at 10 N load for Inconel 718 towards silicon carbide  $1.5 \times 10^{-3} \text{mm}^3\text{N}^{-1}\text{m}^{-1}$ . Minimum wear price occurs at 40 N load for Inconel 718 in opposition to silicon carbide this is  $0.4800 \times 10^{-3} \text{mm}^3\text{N}^{-1}\text{m}^{-1}$ .

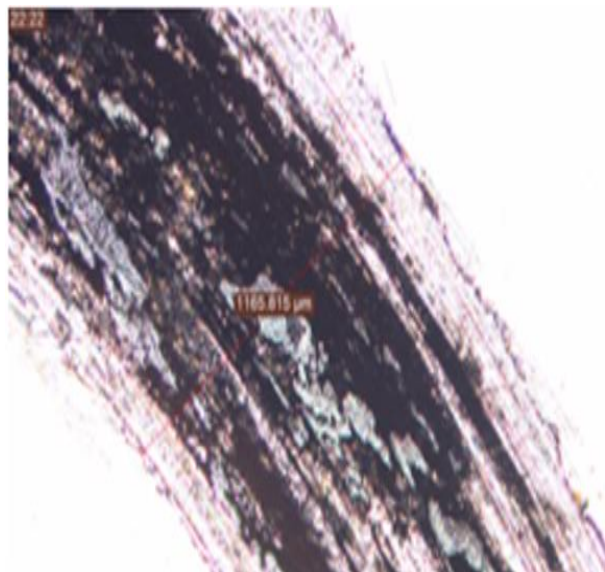


**Figure 3:** Wear rate of Inconel 718 disc as a function of load

The table 4 also represents the records that offers the variation of damage charge of silicon carbide balls towards Inconel 718 under equal test situations. The Figure 4 represents the variation of wear price of silicon carbide balls against Inconel 718. The variety of wear and tear rate for silicon carbide balls in opposition to Inconel 718 is in between  $(2.82-1.95) \times 10^{-6} \text{ mm}^3/\text{N-m}$ . Maximum put on price arise at 10 N load for silicon carbide balls towards Inconel 718 is  $2.82 \times 10^{-6} \text{ mm}^3/\text{N-m}$ . Minimum wear fee occur at 20 N load for silicon carbide balls in opposition to Inconel 718 is  $0.846 \times 10^{-6} \text{ mm}^3/\text{N-m}$ .

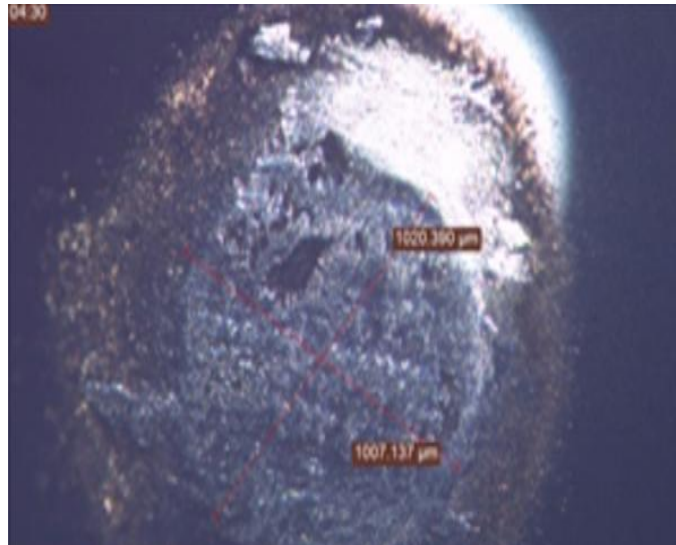


**Figure 4:** Wear rate of Silicon carbide balls against Inconel 718 and Nimonic 80A as a function of load.

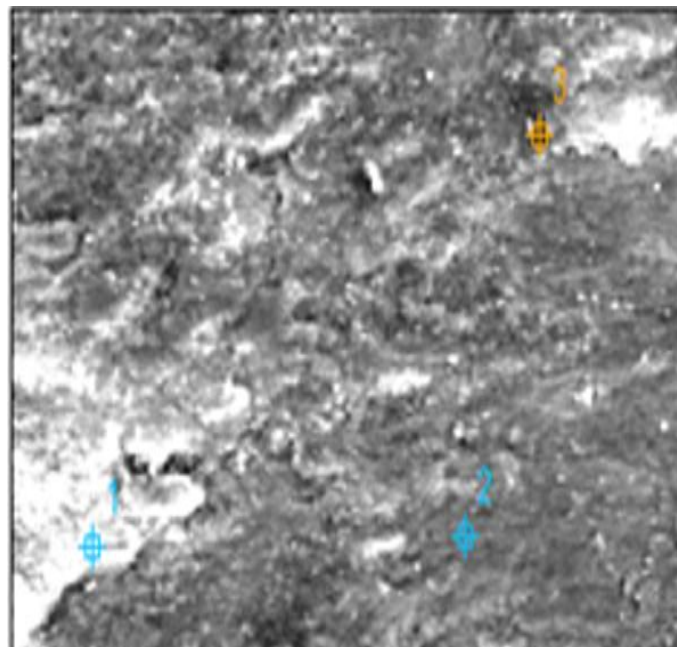


(a)





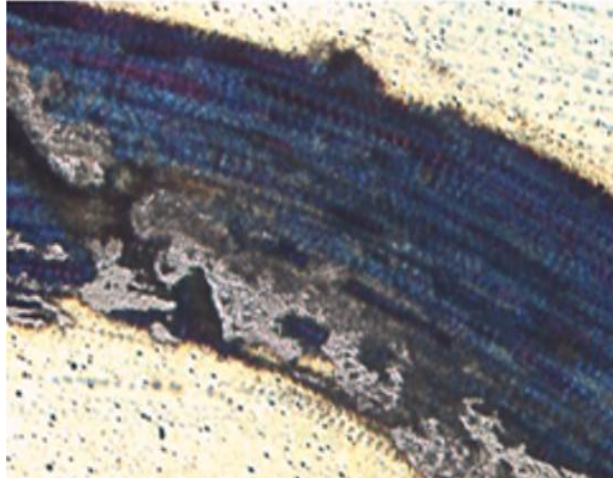
(b)



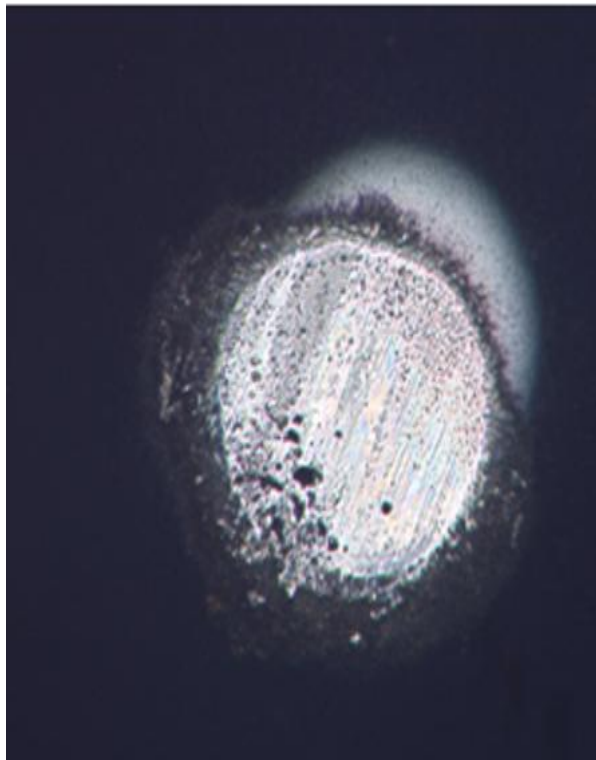
(c)

**Figure 5:** (a) Optical image of wear scar of Inconel 718 (b) Optical image of wear scar of silicon carbide ball (c) EDX and SEM images of scar at 10N for Inconel 718 against silicon carbide ball.

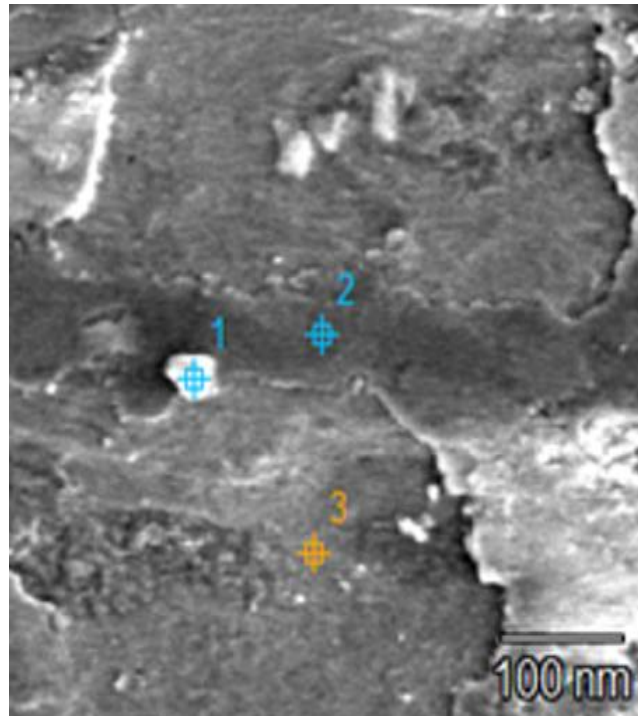




(a)

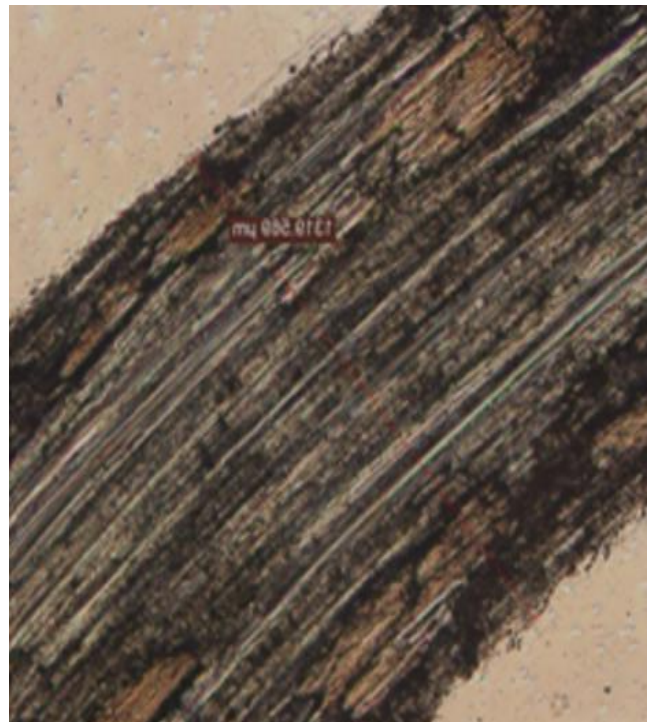


(b)

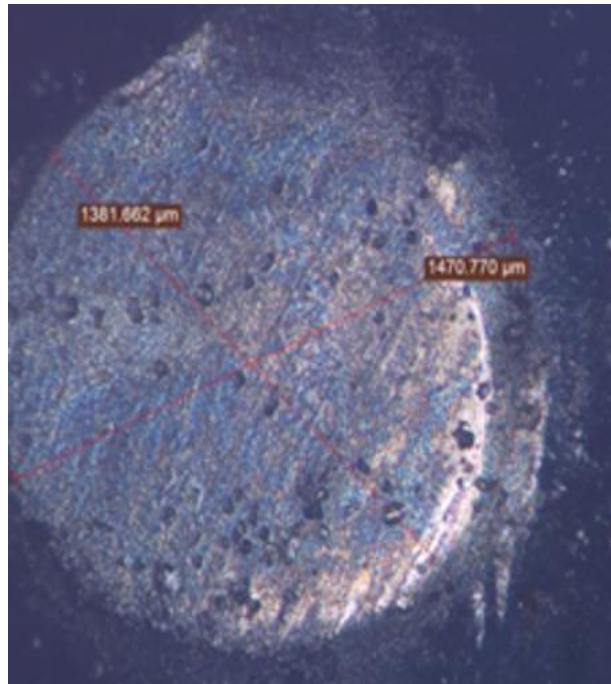


(c)

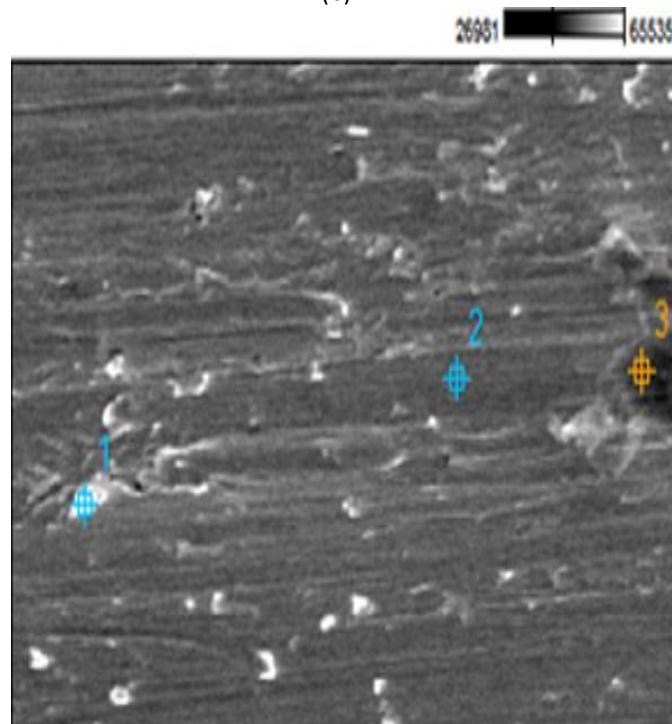
**Figure 6:** (a) Optical image of wear scar of Inconel 718 (b) Optical image of wear scar of silicon carbide ball (c) EDX and SEM images of scar at 20N for Inconel 718 against silicon carbide ball.



(a)

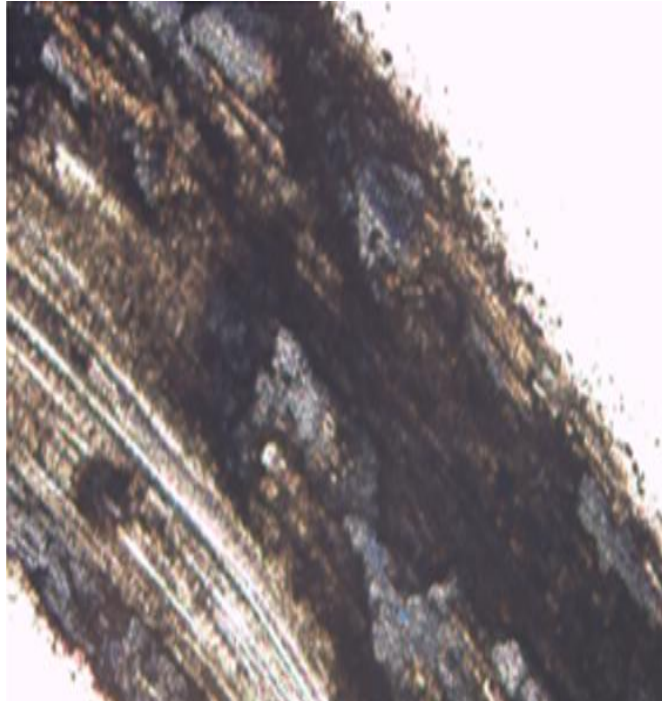


(b)

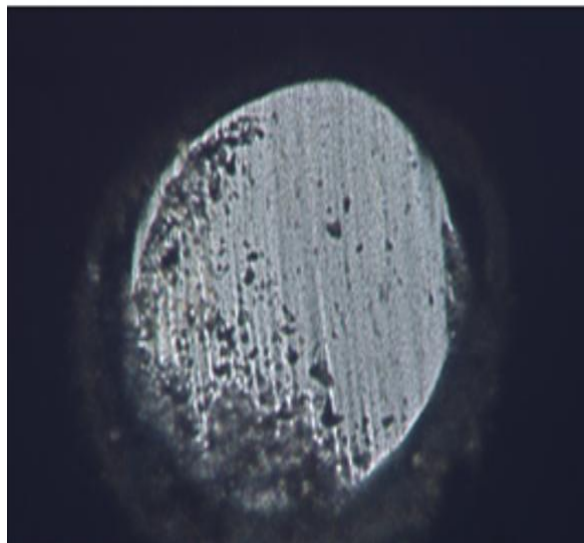


(c)

**Figure 7:** (a) Optical image of wear scar of Inconel 718 (b) Optical image of wear scar of silicon carbide ball (c) EDX and SEM images of scar at 30N for Inconel 718 against silicon carbide ball.

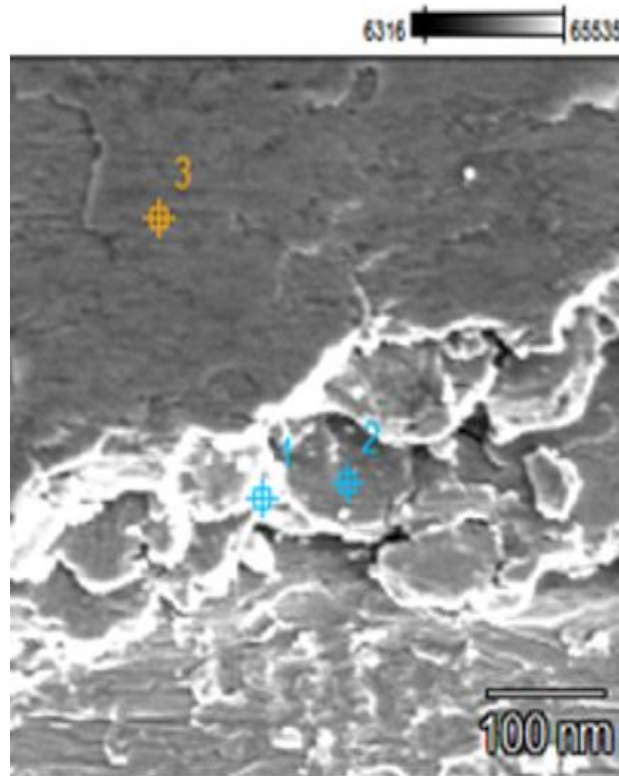


(a)



(b)





(c)

**Figure 8:** (a) Optical image of wear scar of Inconel 718 (b) Optical image of wear scar of silicon carbide ball (c) EDX and SEM images of scar at 40N for Inconel 718 against silicon carbide ball

## VIII. CONCLUSION

The present research investigates the effect of friction and put on conduct of Inconel 718 against silicon carbide tribo pair slide at constant sliding pace of 0.111m/s (sliding ball on disc arrangement) as opposed to load and the effects are concluded as:

The coefficient of friction will increase with growth in load because the load will increase from 30 N to 40 N the oxide layer will become thicker and consequences within the expanded coefficient of friction. The damage fee of sample decreases with increase in load and counter face has lowering trend with growth in load. From the above outcomes and dialogue, it could be concluded that the tribopair with Inconel 718 used in this study offers higher consequences as examine to different tremendous alloy tribopair as studied by way of various researchers.

## REFERENCES

- [1]. Gwidon W. Stachowiak, Andrew W. Batchelor, Engineering tribology, fourth edition. pages 2-5.
- [2]. K.G. Thirugnanasambantham, S. Natarajan, mechanistic studies on degradation in sliding wear behavior of IN718 and Hastelloy X superalloys at 500 °C tribology International, Volume 101, September 2016, Pages 324-330.
- [3]. A. Pauschitz, M. Roy, F.Franek, mechanisms of sliding wear of metals and alloys at elevated temperatures, Tribol.Int.41(2008) 584-602.
- [4]. Y. Birol, High temperature sliding wear behaviour of Inconel 617 and m Stellite 6 alloys, Wear, 269 (2010), pp. 664–671.
- [5]. H.Ackermann, G.T.Kosseva, k.Lucka, H.Koehne, S.Richter, J.Mayer, oxidation behavior of selected wrought Ni-base high temperature alloy when used as flame tube material in modern blue flame oil burners,Corros.Sci.49(2007)3866-3879.
- [6]. Changming Huang, Bin Zou, Peng Guo, Yanan Liu, Chuanzen Huang, Jun Wang sliding behavior and wear mechanism of iron and cobalt-based high-temperature alloys against WC and SiC balls International Journal of Refractory Metals and Hard Materials, Volume 59, September 2016, Pages 40-55.
- [7]. J.M.Zhen, F.Li., S.Y.Zhu, J.Q.Ma, H.Qiao, W.M.Liu, Friction and wear behavior of nickel-alloy-based high temperature self-lubricating composites against Si3N4 and Inconel 718,Tribol.Int.75 (2014) 1-9.
- [8]. T.Sugihara,T.Eenomoto,High speed machining of Inconel 718 focusing on tool surface topography of CBN tool, Proc.Manuf.1(2015) 675-682.
- [9]. Xiao, Wei-han, Shi-qiang Lu, Ya-chao Wang, and S. H. I. Jing. "Mechanical and tribological behaviors of graphene/Inconel718composites." Transactions of Nonferrous Metals Society of China 28, no. 10 (2018): 1958-1969.

- [10]. Courbon, C., F. Pusavec, F. Dumont, J. Rech, and J. Kopac. "Influence of cryogenic lubrication on the tribological properties of Ti6Al4V and Inconel 718 alloys under extreme contact conditions." *Lubrication Science* 26, no. 5 (2014): 315-326.
- [11]. Kim, Sang Hoon, Gi-Hun Shin, Byoung-Kee Kim, Kyung Tae Kim, Dong-Yeol Yang, Clodualdo Aranas, Joon-Phil Choi, and Ji-Hun Yu. "Thermo-mechanical improvement of Inconel 718 using ex situ boron nitride-reinforced composites processed by laser powder bed fusion." *Scientific reports* 7, no. 1 (2017): 14359.
- [12]. Singh, Varshni, and Efstathios I. Meletis. "Synthesis, characterization and properties of intensified plasma-assisted nitrided superalloy Inconel 718." *Surface and Coatings Technology* 201, no. 3-4 (2006): 1093-1101.
- [13]. Attia, Helmi, Salar Tavakoli, Raul Vargas, and Vincent Thomson. "Laser-assisted high-speed finish turning of superalloy Inconel 718 under dry conditions." *CIRP annals* 59, no. 1 (2010): 83-88.
- [14]. Zhen, Jinming, Fei Li, Shengyu Zhu, Jiqiang Ma, Zhuhui Qiao, Weimin Liu, and Jun Yang. "Friction and wear behavior of nickel-alloy-based high temperature self-lubricating composites against Si<sub>3</sub>N<sub>4</sub> and Inconel 718." *Tribology International* 75 (2014): 1-9.
- [15]. Gupta, S., S. Amini, D. Filimonov, T. Palanisamy, T. El-Raghy, and M. W. Barsoum. "Tribological behavior of Ti<sub>2</sub>SC at ambient and elevated temperatures." *Journal of the American Ceramic Society* 90, no. 11 (2007): 3566-3571.
- [16]. Rynio, C., Hattendorf, H., Klower, J., Eggeler, G.: On the physical nature of tribo-layers and wear debris after sliding wear in a super alloy/steel tribo system at 25 and 573 K. *Wear* 317, 26–38 (2014).
- [17]. Gill, S.P.A., McColvin, G., Strang, A.: Stress relaxation of nickel-based super alloy helical springs at high temperatures. *Mater.Sci.Eng.A* 613, 117–129 (2014).
- [18]. Liu, J.K., Cao, J., Lin, X.T., Song, X.G., Feng, J.C.: Microstructure and mechanical properties of diffusion bonded single crystal to polycrystalline Ni-based super alloys joint. *Mater. Des.* 49, 622–626 (2013).
- [19]. J.M.Zhen, F.Li., S.Y.Zhu, J.Q.Ma, z.H.Qiao, W.M.Liu, Friction and wear behavior of nickel-alloy-based high temperature self-lubricating composites against Si<sub>3</sub>N<sub>4</sub> and inconel 718, *Tribol.Int.* 75 (2014) 1-9.